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# 4X4 CIRCULAR PATCH PHASED ARRAY FOR AIRBORNE APPLICATIONS

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# ABSTRACT

This paper concentrates on design, modeling, simulation and performance analysis of a Microstrip Line Quarter Wave Transformer-fed 4x4 Circular Patch phased array. The substrate material RTDuorid5880 used for this has thickness of 1.588mm and relative permittivity ( $\epsilon$ r) is 2.2. The design frequency is 2GHz and VSWR  $\leq 2$ . The proposed 4x4 Circular Patch phased array is modeled and simulated by using ANSOFT HFSS 15.0. The gain of this array is 16.963 dB with return loss of -24.91dB. The phased array is steered for 10<sup>0</sup>, 20<sup>0</sup>, 30<sup>0</sup>, 42<sup>0</sup> and 45<sup>0</sup> with a bandwidth of 31.9 MHz. This proposed Phased array is very useful for L band airborne applications such as satellite navigation, mobile wireless communication, radar and telemetry, tracking, and command (TTC) for mini satellites.

Keywords: Quarter Wave Transformer, RTDuorid5880, Circular Patch, Return Loss.

# 1. INTRODUCTION

In recent Years, the phased array antenna technology an emerging technology day to day, there has been an increasing demand for high gain and narrow beam antennas in the fields of communication as well as the radar. The high gain is used for long distance communication and the narrow beam is useful for finding the direction of the system. The beam scanning or steering is needed to search the object or target in a given volume of the space.

These general limitations with the mechanical scanning. In mechanical scanning, the entire antenna system should be mechanically rotated to steer the beam form one position to another. A practical limitation encountered with the mechanical inertia of the antenna and angular accelerations in re positioning beam, these gives rise to distortion in the radiation.

To overcome these limitations one has to go for electronic scanning for electronic beam scanning in which no mechanical inertia is involved. The method of positioning an electromagnetic beam in space by electric means with the antenna aperture physically remaining fixed is called *electronic scanning* or *electronic beam steering*.

There is a need for beam steering to perform different function modes of an aircraft like ground

mapping for navigation, search and track of ground and air targets.

Phased array antennas with beam steering capability attractive not only sophisticated applications but also in terms of low power consumption in radar and wireless communication application. In electronic beam steering the signal is transmitted in the desired direction hence there is no interference.

# 2. LITERATURE SURVEY

Microstrip antennas are one of the most popular geometries because they are light weight occupies less volume, inexpensive to fabricate and can be easily made conformal to the host body like air craft, space craft, missiles and satellites.. The attractive features of the microstrip enhanced their application in the recent past and stimulated an ever increasing attention from all around to investigate their performance further. Of all the shapes of the microstrip radiator the circular patch tends to be smaller than other configurations. In some applications, such as arrays, circular geometries provide certain advantages over others, since the feed can be connected at any point along the periphery of the circular microstrip. The circular patch is matched to  $50\Omega$  feed line via quarter wave transformer [1-3].

Klaus slobach [4] presented a research paper on Phased Array Simulation Using Circular Patch 28<sup>th</sup> February 2017. Vol.95. No 4 © 2005 – ongoing JATIT & LLS

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Radiators,. In this paper, it was shown practical circular patch radiators may exhibit usual scanning properties in a planar phased array configuration. In this paper it is concluded that small array provides reliable results for scanning angles greater than 600 off broadside. The principal method of investigation is the small array using 8x8 element, but two waveguide simulators were used to check the results.

Frank W. CIPOLLA [5] was investigated on A 7.5 GHz Microstrip Phased for Aircraft for aircraftto-Satellite communication. In this paper, the maximum size of the proposed antenna array of 8x8 rectangular lattice is 17.9x16.3 cm. the gain of the proposed antenna is 20dBic and bandwidth 500MHz. the beam is steered to 600 when the spacing between the elements is  $0.51\lambda$  and it is steered to 450 when the spacing between the elements is  $0.56\lambda$ .

Greg Zomchek, Sharad laxpati [6] presented on s-band phased array for satellite applications. A microstrip Wilkinson splitter followed by a quearter wave transformer was designed and integrated with dual feed square patch in HFASS to provide LHCP Centered at 2.78GHz resulting in an 8.7% bandwidth and the beamwidth is steered in  $\pm 120$ . An s-band phased array was designed for communication between a satellite in geostationary orbit and spacecraft in lower earth orbit.

A research paper on Design and analysis of high gain millimeter wave microstrip antenna array for wireless applications by K. Shambavi, Zachariah C Alex, T. Naveen Phani Krishna[7]. A tranmission line model is used to design antenna array and simulated using IE3d software. The proposed antenna array of 8x8 able to gice a maximum gain of 18.48 dB and beamwidth of 10.490.

A research paper, presented by P. Sai Vinay Kumar, P. Jagadamba, M.N. Giri Prasad [8] on a phased antenna arrays of 4x4 square grid with circular patch for radar applications designed at 1.35 GHz frequency. The antenna array simulations are carried out by using HFSS software. In this paper the proposed phased antenna steered  $\pm 10^{\circ}$  in elevation direction and are useful for many types of applications such as Satellite navigation. Telecommunications. Aircraft surveillance. Amateur radio, Digital Audio Broadcasting and Astronomy.

The main aim of the proposed QWT Fed 4X4 array antenna is to get the high gain, high directivity, high efficiency, narrow beamwidth and

to enhance the beam steering capability from  $0^0$  to  $45^0$  in elevation direction.

#### 3. DESIGN OF PROPOSED CIRCULAR PATCH ANTENNA

The design of the circular microstrip patch array begins with single element. The circular microstrip patch antenna design can be divided into three stages, namely design of the circular patch, the quarter wave transformer and the microstrip feed line. Each of these stages is presented in detail below.

# 2.1 Design of Circular Patch

# Radius of the patch:

The radius 'R' of the circular patch can be found from the following equation [3]:

$$R = \frac{F}{\left[1 + \frac{2h}{\pi \varepsilon_r F \left[ln\left(\frac{F\pi}{2h}\right) + 1.7726\right]}\right]^{1/2}}$$
(1)  
Where  $F = \frac{8.791X10^9}{f_T \sqrt{\varepsilon_r}}$ 

R = radius of the patch in mm;

h = height of the patch substrate in mm;

 $f_r$  = resonant frequency in Hz;

 $\varepsilon_r$  = effective dielectric constant of the substrate.

Using the above expression the calculated radius is 28.52 mm for 2 GHz operating frequency, with RTDuorid5880 substrate having dielectric constant of 2.2 and height of the substrate is 1.588 mm.

# 2.2 Design of the Quarter wave Transformer

Impedance matching is an important aspect in the design of microwave and millimeter circuitry since impedance mismatch may severally deteriorate the overall performance of electronic system. Impedance matching is necessary for the best possible energy transfer from stage to stage. Consider a transmission line with characteristic impedance  $Z_o$  with a resistive load  $R_L$  as shown in Figure 1. If  $Z_o = R_L$  then the maximum power delivered to the load.



Figure 1: Transmission Terminated with Resistive Load

If  $Z_o \neq R_L$ , then we have to use a matching network in the transmission line. There are different methods to match the source impedance

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with the load. They are L Network, single stub tuners and quarter wave transformers. A Quarter Wave Transformer (QWT) whose length is <sup>1</sup>/<sub>4</sub> of wave length is a simple and useful device for matching real load impedance to source impedance as shown in Figure 2.



Figure 2: Transmission Line with Matching Network (QWT)

Similarly we can design microstrip line QWT to match  $50\Omega$  line and the circular patch as shown in Figure 3.



Figure 3: Circular Patch Matched with Feed Line Via QWT Microstrip Line

The input impedance of the QWT is geometric average of the  $Z_0$  and  $R_L$ . [11]

$$Z_{\rm T} = \sqrt{(Z_{\rm o}R_{\rm L})} \tag{2}$$

Where

 $Z_0$  = Characteristic Impedance of the Feed Line =  $50\Omega$ 

 $R_L$  = Input impedance of the circular patch = 340 $\Omega$ 

From the above values the calculated impedance of QWT is  $130\Omega$ .

#### 2.3 Design of a Microstrip line feed

To excite the circular microstrip patch, a 50 $\Omega$  microstrip line is used. The widths of the QWT & microstrip line calculated with the known values  $Z_T=130\Omega$ ,  $Z_o=50\Omega$  and dielectric constant of the substrate  $\varepsilon_r$  (2.2) using the standard equations is given below [12].

$$\frac{w_f}{h} = \begin{cases} e^{\frac{8\pi^4}{\varepsilon^{2A-2}}} & for \frac{w_f}{h} < 2\\ \frac{2}{\pi} \left[ B - 1 - \ln(2B - 1) + \frac{\varepsilon_f - 1}{\varepsilon_f + 1} \left\{ \ln(B - 1) + 0.39 - \frac{0.61}{\varepsilon_f} \right\} \right] for for \frac{w_f}{h} > 2 \end{cases}$$

$$Where A = \frac{Z_0}{\varepsilon_0} \sqrt{\frac{\varepsilon_f + 1}{2}} + \frac{\varepsilon_f - 1}{\varepsilon_f + 1} (0.23 + \frac{0.11}{\varepsilon_f}) \qquad (4)$$

$$and B = \frac{377 \pi}{2Z_0 \sqrt{\varepsilon_f}}$$

The calculated widths of  $50\Omega$  microstrip line and QWT is 4mm and 0.7mm respectively

Dimensions of proposed single circular patch antenna is given in Table 1

TABLE 1: Calculated	Dimensions	of Proposed	Single
	CPA		

Parameter	Value(mm)
Radius of CPA (R)	28.52
Height of the substrate (h)	1.588
Length of the substrate $(L_s)$	138.52
Width of the substrate (W <sub>s</sub> )	60
Length of QWT (L <sub>tr</sub> )	28.62
Width of the QWT $(W_{tr})$	0.74
Length of the feed line (L <sub>f</sub> )	10
Width of the feed line (W <sub>f</sub> )	4

The geometry of the proposed circular patch antenna fed with QWT is shown in Figure 4.



Figure 4: Geometry of the Circular Patch Antenna

The modeled structure of single circular patch antenna is as shown in Figure 5 with a maximum size of antenna as 200mmX350mmX24mm.



Figure 5: Structure of Modeled Single Circular Patch Antenna.

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#### 4. DESIGN AND ANALYSIS OF 4X4 CIRCULAR PATCH PHASED ARRAY ANTENNA

The array factor for N elements in general is [10]

$$AF = \left[\frac{1}{M} \frac{\sin\left(\frac{M\Psi_{\chi}}{2}\right)}{\sin\left(\frac{\Psi_{\chi}}{2}\right)}\right] \left[\frac{1}{N} \frac{\sin\left(\frac{N\Psi_{y}}{2}\right)}{\sin\left(\frac{\Psi_{y}}{2}\right)}\right]$$
(6)

Where

$$\Psi_{x} = kd_{x}sin\theta \cos\phi + \beta_{x}$$
$$\Psi_{y} = kd_{y}sin\theta \cos\phi + \beta_{y}$$

The direction of the major radiation from an array can be controlled by changing the phase excitation between the elements. It is then logical to assume that the maximum radiation can be oriented in any direction to form a scanning array.

The single QWT fed circular patch antenna is used as the array element for this 4x4 planar array. The spacing between elements in X-direction 100mm and Y-direction 150mm is maintained to get desired radiation characteristics. All the elements are fed with the same amplitude and difference in phase. The structure of modeled and simulated 4x4 circular patch phased array antenna is shown in Figure 6.



Figure 6: 4x4 Circular Patch Phased Array

# 5. SIMULATED RESPONSE OF 4X4 CIRCULAR PATCH PHASED ARRAY ANTENNA

The simulated return loss, VSWR and Bandwidth of the proposed QWT Fed 4x4 Circular Patch Phased Array are as shown in Figure 7-9.



Figure 7: Simulated Return loss of 4x4 Circular Patch Phased Array

Return loss is a measure of the reflected energy from a transmitted signal. It is a logarithmic ratio measured in dB (decibel) that compares the power reflected by the antenna to the power that is fed into the antenna from the transmission line.

The larger the value of return loss the less is the energy reflected. For good impedance matching resonant frequency must lie below -10dB.

The obtained return loss of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is -24.91dB.



Figure 8: Simulated VSWR of 4x4 Circular Patch Phased Array

VSWR stands for Voltage Standing Wave Ratio. VSWR is a measure of matched impedance. The parameter VSWR is a measure that numerically describes how well the antenna is impedance matched to the radio or transmission line it is connected to. The smaller the VSWR the better the antenna matched to the transmission line and the more the power delivered to the antenna. For the perfect matching VSWR = 1, there is no reflection and return loss. In the real system it is very hard to achieve a perfect match, so it is defined that having VSWR < 2 is good matching system.

The obtained VSWR of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is 1.1872.

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Figure 9: Simulated Bandwidth of 4x4 Circular Patch Phased Array

The Bandwidth is defined as the range of frequencies over which antenna parameters like bandwidth, gain input impedance, VSER, Beamwidth, VSWR and are within the specified value are called bandwidth. It is the range between upper cut-off frequency and lower cut-off frequency at -10 dB. Bandwidth indicates range of frequency for which an antenna provides satisfactory operation

The obtained Bandwidth of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is Bandwidth 31.9MHz.

The simulated gain, directivity efficiency and half-power beam widths in both elevation and azimuth directions of the proposed QWT Fed 4x4 Circular Patch Phased Array are as shown in Figure10-14.



Figure 10: Simulated Gain of 4x4 Circular Patch Phased Array

Gain is a measure of the ability of the antenna to direct the input power into radiation in a particular direction and is measured at the peak radiation intensity. The gain of an antenna in a given direction is the amount of energy radiated in that direction compared to the energy an isotropic antenna would radiate in the same direction when driven with the same input power. The gain of the antenna is depends on the aperture size.

The obtained gain of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is 16.963 dB



Figure 11: Simulated Directivity of 4x4 Circular Patch Phased Array

Directivity of an antenna is a measure of the concentration of the radiated power in a particular direction. If the antenna had 100% radiation efficiency, all directivity would be converted to gain. The directivity is depends on the radiation pattern of the antenna.

The obtained directivity of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is 17.106 dB



Figure 12: Simulated Efficiency of 4x4 Circular Patch Phased Array

Efficiency is the ratio of power actually radiated to the power put into the antenna terminals. It also can be calculated as radiation resistance divided by total resistance. A high efficiency antenna has the most power present at the antenna's input radiated away whereas a low efficiency antenna has most of the power absorbed as losses within the antenna. The losses within an antenna are usually the conduction losses and dielectric losses.

The obtained efficiency of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is is 98%



Figure 13: Simulated Elevation HPBW of Circular Patch Phased Array.

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The angle between the points in the main lobe that are down from the maximum gain by 3 dB is called Beamwidth. It is also known as the Half Power Beamwidth (HPBW) is typically defined for each of the principle planes.

The obtained elevation half power beam width (HPBW) of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is  $21.4357^{\circ}$ .



Figure 14: Simulated Azimuth HPBW Of Circular Patch Phased Array.

The obtained Azimuth half power beam width of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna at 2GHz is  $12.7756^{\circ}$ .

## 6. BEAM STEERING OF 4X4 CIRCULAR PATCH PHASED ARRAY

The proposed phased array is steered at an angle of  $10^{0}$ ,  $20^{0}$ ,  $30^{0}$ ,  $42^{0}$  and  $45^{0}$  in elevation direction by changing the progressive phase between the elements.

The phase difference between the elements in both the directions is  $60^{\circ}$ , the elevation beam is steered at  $10^{\circ}$  with a Half Power Beam Width (HPBW) of 18.8374° as shown in Figure 15.



Figure 15: Simulated Elevation Beam Steered At  $10^{\circ}$ .

The phase difference between the elements in both the directions is  $122^{\circ}$  and the elevation beam is steered at  $20^{\circ}$  with a HPBW of  $22.8786^{\circ}$  as shown in Figure 16.



Figure 16: Simulated Elevation Beam Steered At  $20^{\circ}$ .

The phase difference between the elements in both the directions is  $156^{\circ}$  and the elevation beam is steered at  $30^{\circ}$  with a HPBW of  $21.6690^{\circ}$  as shown in Figure 17.



*Figure 17: Simulated Elevation Beam Steered At*  $30^{\circ}$ *.* 

The phase difference between the elements in both the directions is  $178^{\circ}$  and the elevation beam is steered at  $42^{\circ}$  with a HPBW of 24.9619° as shown in Figure 18.



*Figure 18: Simulated Elevation Beam Steered At*  $42^{0}$ *.* 

The phase difference between the elements in both the directions is  $180^{\circ}$  and the elevation beam is steered at  $45^{\circ}$  with a HPBW of  $25.3121^{\circ}$  as shown in Figure 19.



*Figure 19: Simulated Elevation Beam Steered At 45<sup>0</sup>.* 

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## 7. DISCUSSION

The proposed 4x4 phased array is successfully modeled and simulated by using ANSOFT HFSS 15.0 and the radiation characteristics of array are as summarized in the table 1.

TABLE 2. Rad	iation charac	teristics of t	he nronosed	CPA
INDLL 2. Ruu	iunon churuc	i $c$ $i$ $s$ $i$ $c$ $s$ $o$ $j$ $i$	ne proposeu	CI II

S.No.	Parameter	Value
1	Frequency	2 GHZ
2	VSWR	1.1872
3	Return loss	-24.9163dB
4	Bandwidth	31.9 MHZ
5	Gain	16.963 dB
6	Directivity	17.106dB
7	Efficiency	98%
8	Elevation HPBW	21.4357 <sup>0</sup>
9	Azimuth HPBW	$12.7756^{0}$

The phased array is also steered for  $10^{0}$ ,  $20^{0}$ ,  $30^{0}$ ,  $42^{0}$  and  $45^{0}$  by changing the progressive phase between the elements and the beamwidth are discussed in below table 3.

TABLE 3: Beamsteering Angles and Elevation Hal	f
Power Beamwidths	

S.No	Beamsteering Angle	Elevation Half Power Beamwidth
1	$10^{0}$	$18.8374^{0}$
2	$20^{0}$	$22.8786^{0}$
3	$30^{0}$	$21.6690^{\circ}$
4	$42^{0}$	$24.9619^{0}$
5	$45^{0}$	$25.3121^{\circ}$

The following table 4 shows the comparison of various antenna parameters like return loss, gain, bandwidth and directivity of the existing methods with the proposed method.

 

 TABLE 4: Comparison of Proposed array results with Reference papers

Parameters	Gain (dB)	Return Loss (dB)	Band Width (MHz)	Directivity (dB)
Paper-1 [15]	14.81	-29.94	1468	17.56
Paper-2 [16]	14.84	-27.1	150	-
Paper-3 [17]	16.02	-29.85	-	-
Proposed Antenna	16.96	-24.91	31.9	17.106

From the above table the gain of the proposed QWT Fed 4x4 Circular Patch Phased Array antenna is 16.96dB, which is highest compare to other papers. As gain increases the distance between

transmitter receiver increases, which can be used for long distance communications.

## 8. ADVANTAGES

The main advantage of the proposed work includes High Gain, High directivity, Narrow beamwidth, Highest efficiency, Light weight and low volume, Low profile planar configuration which can be easily made conformal to host surface, Low fabrication cost, hence can be manufactured in large quantities and Supports both, linear as well as circular polarization.

#### 9. APPLICATIONS

The proposed QWT Fed 4x4 Circular Patch Phased Array antenna can be used in Airborne Applications such as Wireless Mobile communication, Satellite navigation Systems, radar and telemetry, tracking, and command (TTC) for mini satellites.

#### **10. CONCLUSION**

4x4 Circular Patch Phased Array was designed and successfully simulated. The gain of proposed array is 16.963 dB, VSWR is 1.1872, return loss is -24.9163 dB, Bandwidth is 31.9 MHz, elevation HPBW is 21.4357<sup>0</sup>, Azimuth HPBW is 12.7756<sup>0</sup> and the elevation beam is steered in various directions for various phase angles. The radiation characteristics obtained for the proposed array is very much useful for L band airborne applications such as satellite navigation, mobile wireless communication, radar and *telemetry*, *tracking*, and command (TTC) for mini satellites.

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