20th September 2015. Vol.79. No.2

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ISSN: 1992-8645

www.jatit.org



E-ISSN: 1817-3195

# DESIGN A SQUARE MICROSTRIP PATCH ANTENNA AT 2.4 GHZ, AND COMPARISON BETWEEN UNSLOTTED AND SLOTTED VERSION

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### ABSTRACT

Low profile antennas support the operation of many modern communication systems. Microstrip patch antennas represent one family of compact antennas that offer a conformal nature and the capability of ready integration with communication system's printed circuitry. And it has many advantages over conventional antennas. In this paper a square Microstrip Patch Antenna has been designed at 2.4 GHz frequency. By using Microwave office 2006 software (AWR) for design simulation to get the best parametric design, and compared with a slotted version of the antenna having a slotting shape of letter (P). It included in the design the return loss, gain, radiation pattern, bandwidth, HPBW, co and cross polar isolation parameters. The square slotted antenna that designed has a result of a return loss is about (-42.41dB) and about 12.92% bandwidth.

#### Keywords: Return Loss, Coaxial Feed, Bandwidth, Antenna Radiation Pattern, Co-Polar Isolation, Cross-Polar Isolation.

## 1. INTRODUCTION

Microstrip antennas (MSAs) are used in a broad range of applications from communication systems to biomedical systems, primarily due to several attractive properties such as light weight, low profile, low production cost, conformability, reproducibility, reliability, and ease in fabrication and integration with solid state devices. In recent years the rapid decrease in size of personal communication devices has lead to the need for more compact antennas. As communication devices become smaller due to greater integration of electronics, the antenna becomes a significantly larger part of the overall package volume. Presently there are many other government and commercial applications, such as mobile radio and wireless communications that use microstrip antennas [1] [2].

Microstrip antennas however have limitations in terms of bandwidth and efficiency, all imposed by the very presence of the dielectric substrate. The following drawing shows a patch antenna and its basic form: a flat plate over a ground plane, the center conductor of a coax serves as the feed probe to couple electromagnetic energy in and/or out of the patch [3].



#### Figure 1: Shows The Form Of The Microstrip Patch Antenna

In its most basic form, a microstrip patch antenna consists of a radiating patch on one side of a dielectric substrate which has a ground plane on the other side. The patch is generally made of conducting material such as copper or gold and can take any possible shape. The radiating patch and the

Journal of	Theoretical	and Applied	Information	Technology

20<sup>th</sup> September 2015. Vol.79. No.2

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ISSN: 1992-8645	www.jatit.org	E-ISSN: 1817-3195

feed lines are usually photo etched on the dielectric substrate [4].

Microstrip patch antennas can be fed by a variety of methods. These methods can be classified into two categories-contacting and non-contacting [5].

In the contacting method, the RF power is fed directly to the radiating patch using a connecting element such as a microstrip line. In the noncontacting scheme, electromagnetic field coupling is done to transfer power between the microstrip line and the radiating patch. The four most popular feed techniques used are the microstrip line, coaxial probe, aperture coupling and proximity coupling [6].

In this paper more details mentioned to it such as the dielectric substrate dimensions, feeding contact point dimensions and also the slotted design in our letter (P), it depends on position & size of letter.

And there is another thing also important the (positioning the feeding point), because when we want to get best RL result it must move feeding point randomly until getting a best results, and this is take a lot of time to get it.

#### 2. DESIGN CONSIDERATION

There are many things or parameters that should be putted in consideration before starting the design of microstrip patch antenna, like the length (L), width (W) and the thickness (h) of the patch and also Dielectric constant of the substrate ( $\varepsilon$ r) and the Frequency of operation. And these parameters showed in figure 2.



Figure 2: The Parameters Of The Microstrip Patch Antenna

To start there are two important values in the design must be found, the Width and Length of the patch [7].

Firstly the width can found from the equation (1):

$$W = \frac{C}{2f\sqrt{\frac{\epsilon r+1}{2}}} \tag{1}$$

And the operating frequency (2.4) GHz is given and also the dielectric constant (4.7) that it needs to calculate the width (w).

It founded the width equals approximation: W=37 mm.

Then also must calculate the length, it can be found from the equation (2) [8]:

$$L = \frac{C}{2f\sqrt{\varepsilon r(eff)}} - 2\Delta L \qquad (2)$$

As seen in the above equation it needs to find  $\Delta L$  and  $\epsilon$  reff (Effective dielectric constant), and they can be found from equations (3) and (4) [9].

$$\Delta L = \frac{0.412h[\varepsilon r(eff) + 0.3](\frac{W}{h} + 0.264)}{[\varepsilon r(eff) - 0.258](\frac{W}{h} + 0.8)}$$

(3)

And

$$\varepsilon r(eff) = \frac{(\varepsilon r + 1)}{2} + \frac{(\varepsilon r - 1)}{2\sqrt{\left(1 + \frac{10w}{h}\right)}} \quad (4)$$

From equation (4) having ( $\epsilon r$ ), so easily ( $\epsilon$  reff) can be found, that equals 4.397, and then uses the last one in equation (3) to find  $\Delta L$  that equals 0.731. After that to calculate the length (L) and it will be 28.5 mm.

As seen from the results W=37 mm, and L=28.5 mm. This means the patch is not square, its rectangle. But it must be square. So it will take these measurements in form of (L x L). Means, on square patch it will neglect the value of the width (w).

## Journal of Theoretical and Applied Information Technology

20th September 2015. Vol.79. No.2

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ISSN: 1992-8645

<u>www.jatit.org</u>



E-ISSN: 1817-3195

It should also be mentioned that the thickness of the air gap above the substrate is taken as 16mm which is well known as a practical value (10 times the thickness of the dielectric), and these dimensions have been chosen of the substrate to be **40mmX40mm**, which is bigger than the patch, to be enough, it used **co-axial** as a feeding technique. And the dimensions of feed point is

**0.5mmX0.5mm** have been taken.

In the end after all these measurements, the unslotted patch antenna designed and get the best value of return loss is about (-42.8dB), after moving it randomly and at last get this value, as shown in figure 3.



Figure 3: Un-Slotted Patch Antenna

Now design the slotted version of the same patch above, to implement the letter (P). And here in design also must change the shape of the letter and change it's position of course randomly until we get the best result. The design becomes as shown in figure 4.



Figure 4: Slotted Patch Antenna With Shape Letter (P)

After the slotted patch designed, the return loss and bandwidth must be computed. All of these computations for unslotted and slotted will show in simulation results.

### 3. SIMULATION RESULTS

Firstly it will show the simulation results of the unslotted version. And then it will show the simulation results of the slotted version and compare between them.

The return loss for un-slotted design in the figure below:



Figure 5: Un-Slotted Patch Return Loss

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ISSN: 1992-8645	www.jatit.org	E-ISSN: 1817-3195

From figure 5 above the bandwidth can be calculated (**BW**) in **-10dB** RL in the lower & upper frequencies f1 and f2. Upper frequency was **2.556GHz** while the lower frequency was **2.245GHz** and operation **frequency** was **2.4GHz**. Firstly subtract f1 from f2 and the result divide it by square root of multiplying f1 and f2. And this gives the **BW=12.98%**. As shown in Eq. below

#### BW = (f2-f1)/f

Now from radiation pattern figure below, the other parameters can be calculated.



Figure 6: Un- Slotted Patch Radiation Pattern

The radiation pattern measured in term of (Phi) and  $\theta$  (Theta). Because the radiation pattern is perpendicular to the patch.

And now the Gain calculated and it equals **4.634 dB**. For calculating the HPBW (Half Power Beam Width) which is the maximum angle, and to compute HPBW it should be dropped from **4.634 dB** to **3dB** gain and measure the angle from the top to that position.

Ones in the right side and then in the left side and add them. Founding HPBW has **66.86°**, it gives **33.43°** on each side, because the two sides are symmetrical.

And for the Co-Polar isolation is the same as the top value of what has E-Phi 90° value, which is **4.634 dB**, while the Cross-polar isolation is

calculated by subtracting the top value of E-Phi 90° from the top value of E-Phi 0° which will be:-

#### 4.634 dB - (-12.9 dB) = 17.534 dB

Returning to slotted patch design, and compute the parameters as it had been done in un-slotted patch.



Figure 7: Slotted Patch Return Loss

From figure (7) above the bandwidth can be calculated (**BW**) in -10dB RL in the lower & upper frequencies f1 and f2. Upper frequency was 2.551GHz while the lower frequency was 2.242GHz and operation frequency was 2.4GHz. Firstly subtract f1 from f2 and the result divide it by square root of multiplying f1 and f2. And this gives the **BW= 12.92%**. As shown in Eq. below

### $\mathbf{BW} = (\mathbf{f2} - \mathbf{f1})/\mathbf{f}$

Now from radiation pattern figure below, the other parameters can be calculated.

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ISSN: 1992-8645

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Figure (8), Slotted patch radiation pattern

As obvious from figure above is approximately the same in slotted and un-slotted design. The Gain is **4.647 dB**, the HPBW has **67.3°**. And for the Co-Polar isolation is the same as the top value of what has E-Phi 90° value, which is **4.647 dB**. Cross-polar isolation is calculated by subtracting the top value of E-Phi 90° from the top value of E-Phi 0° which will be:-

### 4.647 - (-12.8 dB) = 17.447 dB

### 4. ANALYSIS AND DISCUSSION

From the results in the slotted and the un-slotted design, as seen before by making slot on the patch and all results, all parameters almost the same as un-slotted. The performance of the antenna that designed not changed very high. And these results depend on the position and size of the slot (P), this position and size have been chosen randomly by trial and error. And every time changing them we get different results. And all results that got of course depend on the other parameters, like dielectric substrate, this must be chosen carefully. And the dimensions of the feeding point also important to choose it and not changed during simulation.

Now in radiation pattern seen in the figures that is no change or approximately the same, HPBW, the Co-Polar isolation and Cross-polar isolation.

In the end the bandwidth BW changed but small decrease as mentioned.

### 5. CONCLUSION

A square microstrip patch antenna was designed at frequency 2.4 GHz. As seen in this paper in the results an important parameters included like feed network and impedance matching in microstrip patch antenna design. And also the affect of changing the position of feed point on the performance of the antenna. And a comparison has made between the un-slotted design and slotted one. And the results discussed if the size and position of letter (P) changed.

### **REFERENCES:**

- [1] Kin-Lu Wong, "Compact and Broadband Microstrip Antennas", *John Wily* & Sons, 2002.
- [2] Bahl, I.J. and Bhartia, P., Microstrip Antennas, Artech House, Dedham, MA, 1990.
- [3] R. B. Waterhouse, "Cross-polarization characteristics of the circular patch antennas," Electron. Lett., 1997.
- [4] J. M. Laheurte, A. Papiernik, and J. R. Mosig, "Modeling of coaxial feed contribution to microstrip antenna impedance: Comparison of a numerical model with analytical expressions," Int. J. Microwave Millimeter Wave CAE, 1993.
- [5] N. Herscovici, "New Considerations in the design of Microstrip Patch Antennas, *IEEE Tram' on Antennas & Propagation*, Vol. 46, June 1998.
- [6] Ting-Hua Liu and Wen Xun Zhang, "Compound techniques for broadening the bandwidth of microstrip patch antenna," Microwave Conference Proceedings, Dec. 1997
- [7] Shakelford, A., Lee, K.F., Chatterjee, D., Guo, Y.X., Luk, K.M., Chair, R., "Small-Size Wide-Bandwidth Microstrip Patch Antennas," Antennas and Propagation Society International Symposium, July 2001.
- [8] Behera, Subhrakanta, and Kalarickaparambil Joseph Vinoy. "Microstrip square ring antenna for dual-band operation." Progress In Electromagnetics Research 93 2009, 41-56.
- [9] Afridi, Muhammad Aamir. "Microstrip Patch Antenna- Designing at 2.4 GHz Frequency." Biological and Chemical Research, 128-132, 2015.