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DYNAMIC ANALYSIS AND OPTIMIZATION DESIGN OF THE SFD- SLIDING BEARING FLEXIBLE ROTOR SYSTEM

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ABSTRACT

The paper proposes a mechanical model of SFD-sliding bearing flexible rotor system, employing Runge-Kutta method to tackle nonlinear differential equation, thus acquiring the dynamic response and the unbalanced response curve. Results obtained show the route of flexible rotor system from stable periodic motion to chaos state is: periodic motion—quasi-periodic motion—chaos —period doubling bifurcation—chaos. The paper analyzes the sensitivity of flexible rotor system, offering design variables to optimization analysis, improving the efficiency of optimization and shortening the design cycle. Based on sensitivity analysis, we conduct optimization analysis on critical speed by the application of genetic algorithm, which aims to further the enlargement of D-value between the first critical speed and the second critical speed. Additionally, the critical speed ameliorates after the optimization which supplies theoretical basis as well as theoretical analysis towards the dynamic stability of high-speed rotor system and provides reference for the design of such rotor system.

Keywords: SFD, Dynamic Analysis, Critical Speed, Sensitivity Theory, Optimization Design

1. INTRODUCTION

The SFD (Squeeze Film Damper), a typical one in the field of rotary mechanical design with the advantage of simple structure, small volume and convenient installation, can effectively afford viscous damping to depress rotor vibration amplitude and diminish external force of the rotor system[1]. Besides, the system dynamic stability improves if reasonable parameters are offered.

Researchers attach importance to SFD due to its excellent vibration reduction effect. Since 1970s, SFD is widely applied in reality and many achievements have been obtained. Nevertheless, certain stimulation about SFD has not been clear until now and still needs further research. So far, engineering design has adopted cut-and-try procedure with the combination of experience, theory and experiment.[2]

This paper establishes the motion equation of the SFD-sliding bearing flexible rotor system, analyzing the system dynamic response; gaining the critical speed of two systems to show the motion state in a visualized way through unbalanced response curve; making use of sensitivity analysis to offer design variables for optimization design; employing genetic algorithm in optimization design to rationalize system parameters and offer reference to the design of such rotor system.

2. MECHANICAL MODEL OF SFD-SLIDING BEARING FLEXIBLE ROTOR SYSTEM

Fig.1(a) and Fig.1(b) represent the structure of SFD-sliding bearing flexible rotor system and its corresponding side view, respectively.[3] Here denotes the center of SFD fixed on rigid support and building coordinate system (inertial reference system), the center of bearing body, constructing integral coordinate system which shifts with the bearing body. The axis passes . is the center of shaft, establishing integral coordinate system which moves with the shaft, with axis passing . Suppose is the center of rotary table.

As shown in Fig. 1, and are film forces that SFD puts on bearing body along axis and axis respectively; while and , film forces which flexible bearing acts on shaft along axis and axis.





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2.1 The Motion Equation of Bearing Center.

The bearing body is mainly affected by SFDacting force, reacting force of axle journal, and gravity, so according to Newton second law, its motion equation can be concluded as Equation (1):

$$m_{1}\ddot{x}_{1} + K_{1}x_{1} = F_{e}\cos j_{1} - F_{t}\sin j_{1} + P_{t}\sin j_{2}$$

- $P_{e}\cos j_{2},$
 $m_{1}\ddot{y} + K_{1}y_{1} = F_{e}\sin j_{1} + F_{t}\cos j_{1} - P_{t}\cos j_{2}$
- $P_{e}\sin j_{2} - m_{1}g.$
(1)

Here x_1 and y_1 are, respectively, the displacements of bearing body center in the X and Y-direction. m_1 is the quality of bearing body, K_1 the rigidity of elastic support in SFD, j_1 the polar angle that integral coordinate system of bearing body $o_1x^{*}y^{*}$ revolves, and j_2 the polar angle that integral coordinate system of axle journal $o_2x^{*}y^{*}$ revolves.

2.2 The Motion Equation of Journal Center.

The shaft is influenced by acting force and gravity of bearing body and rotary table, besides, the flexibility of flexible rotor should be taken into consideration. Based on Newton second law, the motion equation is shown in Equation (2):

$$m_2 \ddot{x}_2 + K_2 (x_2 - x_3) = -P_t \sin j_2 + P_e \cos j_2,$$

$$m_2 \ddot{y}_2 + K_2 (y_2 - y_3) = P_t \cos j_2 + P_e \sin j_2 - m_2 g.$$
(2)

Here x_2 and y_2 are the separately displacements of shaft center on axis x and axis y . m_2 denotes the quality of shaft, K_2 the rigidity of shaft.

2.3 The Motion Equation of Rotary Table Center.

The motion equation can be represented as Equation (3):

$$m_{3}\ddot{x}_{3} + K_{2}(x_{3} - x_{2}) = m_{3}r W^{2} \cos W$$

$$m_{3}\ddot{y}_{3} + K_{2}(y_{3} - y_{2}) = m_{3}r W^{2} \sin W - m_{3}g$$
(3)

Where, x_3 , y_3 are displacements of rotary table center o_3 on axis x and axis y, respectively. m_3 indicates the quality of rotary table, r the mass deviation of rotary table and w the rotational angular speed of rotor.

Given that e is the eccentricity between axle

journal center and bearing body center, e_2 the eccentricity between bearing body center and SFD center, then the geometric relationship between x_1 , x_2 , y_1 , y_2 , j_1 , j_2 can be summarized as Equation (4):

$$\mathbf{e}_{1} = \sqrt{(x_{2} - x_{1})^{2} + (y_{2} - y_{1})^{2}}, \quad \mathbf{e}_{2} = \sqrt{x_{1}^{2} + y_{1}^{2}}$$

$$j_{1} = \arccos \frac{x_{1}}{\mathbf{e}_{2}}, \qquad j_{2} = \arccos \frac{x_{2} - x_{1}}{\mathbf{e}_{1}}.$$
(4)

Adopting long bearing theory to sliding bearing, the expression of film force is [4-5]:

$$P_{e} = 6hR_{1}L_{1} \underbrace{\overset{\otimes}{\overset{\otimes}{e}}_{c_{1}} \overset{\circ}{\overset{\otimes}{\theta}}_{e}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{2\dot{e}_{1}}{\frac{1}{\left(1 - e_{1}^{2}\right)^{3/2}}} \underbrace{\overset{\otimes}{\overset{\otimes}{\theta}}_{e}}^{2} - \frac{8}{p\left(2 + e_{1}^{2}\right)} \underbrace{\overset{\otimes}{\overset{\otimes}{\psi}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{2\dot{e}_{1}}{\frac{1}{\left(1 - e_{1}^{2}\right)^{3/2}}} \underbrace{\overset{\otimes}{\overset{\otimes}{\theta}}_{e}}^{2} - \frac{8}{p\left(2 + e_{1}^{2}\right)} \underbrace{\overset{\otimes}{\overset{\otimes}{\psi}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{\overset{\otimes}{\overset{\otimes}{\theta}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{2\dot{e}_{1}}{\left(1 - e_{1}^{2}\right)^{1/2}\left(2 + e_{1}^{2}\right)} \underbrace{\overset{\otimes}{\overset{\otimes}{\psi}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{2\dot{e}_{1}}{\frac{2e_{1}}{\left(1 - e_{1}^{2}\right)\left(2 + e_{1}^{2}\right)}} \underbrace{\overset{\otimes}{\overset{\otimes}{\psi}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{\dot{e}_{1} \overset{\otimes}{\overset{\otimes}{\theta}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\otimes}{\theta}}} \underbrace{\dot{e}_{1} \overset{\circ}{\overset{\otimes}{\theta}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}_{1} \overset{\circ}{\overset{\otimes}{\theta}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}_{1} \overset{\circ}{\overset{\circ}{\theta}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}_{1} \overset{\circ}{\overset{\circ}{\theta}}}_{\substack{e} c_{1} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \dot{e}} \underbrace{\dot{e}} \dot{e}} \underbrace{\dot{e}} \dot{e}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}} \overset{\circ}{\overset{\circ}{\theta}} \overset{\circ}{\overset{\circ}{\theta}} \underbrace{\dot{e}}$$

Employing short bearing approximation theory for SFD, the expression of film force can be displayed as:

$$F_{e} = \frac{hR_{2}L_{2}^{3}}{c_{2}^{2}} \int_{2}^{2} e_{2} \frac{2e_{2}}{\left(1 - e_{2}^{2}\right)^{2}} + e_{2} \frac{p(1 + 2e_{2})}{2\left(1 - e_{2}^{2}\right)^{5/2}} , \qquad (6)$$

$$F_{t} = \frac{hR_{2}L_{2}^{3}}{c_{2}^{2}} \int_{2}^{2} e_{2} \frac{p}{2\left(1 - e_{2}^{2}\right)^{3/2}} + \dot{e}_{2} \frac{2e_{2}}{2\left(1 - e_{2}^{2}\right)^{2}} , \qquad (6)$$

3. DYNAMIC RESPONSE OF THE FLEXIBLE ROTOR SYSTEM

Table 1: Parameter Values Of The System			
quality of shaft $2 m_2$ (kg)	10		
quality of bearing m_1 (m)	2.5		
bearing radius R_1 (m)	0.005		
bearing width L_{l} (m)	0.01		
bearing clearance c_1 (m)	0.5e-4		
SFD radius R_2 (m)	0.02		
shaft rigidity K_2 (N/m)	2.45e7		
SFD width $L_2(m)$	0.007		
SFD clearance C_2 (m)	0.75e-4		
SFD elastic bearing rigidity K_1 (N/m)	1.75e8		
mass eccentricity r (m)	0.5e-5		

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oil viscosity h (Pa.s)	0.01	in Fig. 4. Further, in Fig. 5 the system does single
gravity acceleration g (m ² /s)	9.8	periodic motion if rotating speed arrives to 960
quality of rotary table m_3 (kg)	0.4	rad/s. When the rotating speed increases, the system comes to chaos again [6-8]



Fig. 5. Dynamic Response While W=960rad/S

The parameters of flexible rotor system can be seen in Table 1. According to calculation, the low rotating speed of rotor results in stable periodic response. Fig. 2 shows the dynamic response when the angular speed is 400rad/s. With the gradual increment of rotating speed, from 400 rad/s to 570 rad/s, the harmonious periodic motion comes to quasi-periodic motion. Fig. 3 reveals the dynamic response at the speed of 900rad/s, when the system is in chaos state. As rotating speed increases to 950 rad/s, the system enters period doubling bifurcation

tem comes to chaos again. [6-8]

SENSITIVITY ANALYSIS ON SFD-4. **SLIDING BEARING FLEXIBLE ROTOR** SYSTEM

During the process of rotational machinery design, the critical speed must be taken into account as a very important parameter. If the working speed is near to critical speed, the system appears large vibration, which causes damage of machine and even threatens people's safety. The critical speed is one of the most significant factors in rotor system design. Most rotors' working speeds are above firstorder, second-order, even multiple-order critical speed. The first critical speed and the second critical speed are of great importance to research on the system stability. It is a remarkable job to change the parameter of rotor system effectively and minimize its variation [9].

In the optimization design of rotational machinery, the parameter sensitive to critical speed is usually chosen, such as structure or bearing. The selection of parameter is determined after sensitivity analysis.

The paper utilizes the ratio between relative variation of critical speed and that of design variable as the relative sensitivity of critical speed, this is:

$$h_{ij}(l,j) = \lim_{\mathsf{D}b_j \circledast 0} \frac{\mathsf{D}a_i / a_i}{\mathsf{D}b_j / b_j} = \frac{b_j \P a_i}{a_i \P b_j}.$$
(7)

where, i = 1, 2, ..., m, l = 1, 2, ..., n. The system sensitivity is critical speed variation caused by the variation of unit configuration parameter (for example, bearing clearance, bearing width, diameter)

Table2 Sensitivity Of The Flexible Rotor System

Design variable	Range of system variables	Sensitivit y of the first critical speed	Sensitivity of the second critical speed
$C_1(\mathbf{m})$	$2e-5 \pounds c_1 \pounds 12e-5$	-0.6714	-0.4752
$L_{1}(\mathbf{m})$	$0.008 \text{\pounds} L_1 \text{\pounds} 0.02$	0.3642	0.1902
R_1 (m)	$2e-3\pounds R_{1}\pounds 7e-3$	-0.2668	-0.1298
$C_2(\mathbf{m})$	5e- 5£ c_2 £ 11e- 5	-0.5314	-0.4808

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$L_2(m)$	$2e-3\pounds L_2\pounds 11e-3$	0.3128	0.0782	5.2 <i>The Selection of Design Variable.</i>
2 < 7				The sensitivity analysis shows that the first
R_2 (m)	$0.01 \text{\pounds} R_2 \text{\pounds} 0.03$	-0.2666	-0.1602	critical speed is sensitive to bearing clearance c_1 ,
K_1 (N/m	$1.55e+8 \pounds K_1 \pounds 4e+9$	0.1325	0.0587	SFD clearance c_2 and oil viscosity h while the
)				second critical speed has high sensitivity towards
$K_2 (N/$	$1.25e7 \pounds K_2 \pounds 4.3e8$	0.0403	0.2390	SFD clearance c_2 , bearing clearance c_1 and shaft
. ′				stiffness K_2 . Therefore, the paper selects bearing
$K_2 (N/m)$ m) h(Pa.s)	1.25e7 £ K_2 £ 4.3e8 0.004 £ h £ 0.016	0.0403	0.2390 0.1805	SFD clearance c_2 , bearing clearance c_1 and

In Table 2, the sensitivity figure is zero dimension and minus sign indicates that the critical speed decreases with design variable increasing. The above table has shown the first critical speed is sensitive to bearing clearance c_1 , SFD clearance c_2 and oil viscosity h while SFD clearance c_2 , bearing clearance c_1 and shaft rigidity K_2 have great influences on the second critical speed and the system is more sensitive to these parameters.

OPTIMIZATION ANALYSIS OF ROTOR 5. SYSTEM

5.1 The selection of Objective Function.

Optimization design needs to determine objective function at first. For rotational machinery, the selection of objective function should be set according to different requirements on the basis of stability. Taken into consideration that the working speed of rotor system should keep away from critical speed within a certain range to avoid resonance vibration which causes destabilization, the working speed should be far from critical speed as much as possible.

Some rotary machines have high working speed which varies in a certain scope between the first critical speed and the second critical speed. In order to avoid the working speed approaching the critical speed, the D-value between the first critical speed and the second critical speed should be enlarged to the utmost, so the objective function is:

$$f(x) = \frac{1}{w_1^2 + w_2^2}.$$
 (8)

Here W_i is the first critical speed of rotor system, W_2 the second critical speed, satisfying $W_1 \pounds W_2$ and the objective is to minimize the function f.

clearance c_1 , SFD clearance c_2 , oil viscosity h and shaft stiffness K_2 as design variables whose constraint ranges are:

$$c_{1\min} \ \pounds \ c_1 \ \pounds \ c_{1\max}, \qquad c_{2\min} \ \pounds \ c_2 \ \pounds \ c_{2\max}, \qquad (9)$$
$$h_{\min} \ \pounds \ h \ \pounds \ h_{\max}, \qquad K_{2\min} \ \pounds \ K_2 \ \pounds \ K_{2\max}.$$

5.3 Analysis of the Optimization Results.

According to the above analysis, the paper employs genetic algorithm to optimize the system. Table 2 indicates the constraint ranges of the design variables.

Table 3 : Change Of Design Variables And Objective Function Before And After Optimization

Variables	Before optimization	After optimization	Rate of change
<i>C</i> ₁ (m)	5e-5	4.1e-5	-18%
<i>c</i> ₂ (m)	7.5e-5	5.7e-5	-24%
h (Pa.s)	0.01	0.014	40%
K_2 (N/m)	2.45e7	2.36e7	-3.6%
f	1.3810e-006	8.1699e-007	-40.8%
W_1 (rad/s)	290	220	-24.14%
W_2 (rad/s)	800	1080	35%
W_2 - W_1 (510	860	68%

The minus sign in the table indicates parameter decreases and if not, the parameter increases. Table 3 shows that the system parameters vary after genetic algorithm: the bearing clearance, SFD clearance and shaft stiffness separately decrease by 18%, 24% and 3.6%, the oil viscosity increase by 40% and the objective function diminishes by 40.8%. With the variation of parameters, the first critical speed reduces, the second critical speed raises and the distance between the two critical speed increases by 68% after optimization.

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Fig. 6. Amplitude Before And After Optimization

In Fig. 6, it is obvious that the distance between the first critical speed and the second critical speed on coordinate axis increases. When the rotating speed is within 410rad/s~880rad/s, the amplitude of rotary machines after optimization is lower than before. Therefore, after optimization, the working speed can be removed from the critical speed to a large extent and at the same time, the amplitude is reduced within the range.

For SFD-sliding bearing flexible rotor system which has variable high rotating speed (the working speed is between the first critical speed and the second critical speed), the distance between the first critical speed and the second critical speed should be enlarged as far as possible, in order to keep the working speed far away from the adjacent two critical speed, thus avoiding resonance vibration effectively.

6. CONCLUSION

The paper has established the mechanical model of SFD-sliding bearing flexible rotor system, analyzing the sensitivity of flexible rotor system on the first two critical speed. This paper has come to the conclusion that the first critical speed is sensitive to SFD clearance, bearing clearance and oil viscosity, which offers design variables to optimization analysis, improves the efficiency of optimization and shortens the design cycle.

Based on design variables offered by sensitivity analysis, this paper has employed genetic algorithm to give an optimization analysis on critical speed, which aims to enlarge the D-value between the first critical speed and the second critical speed to the utmost. The critical speed has ameliorated after the optimization which has remarkable results and provides reference for designers.

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